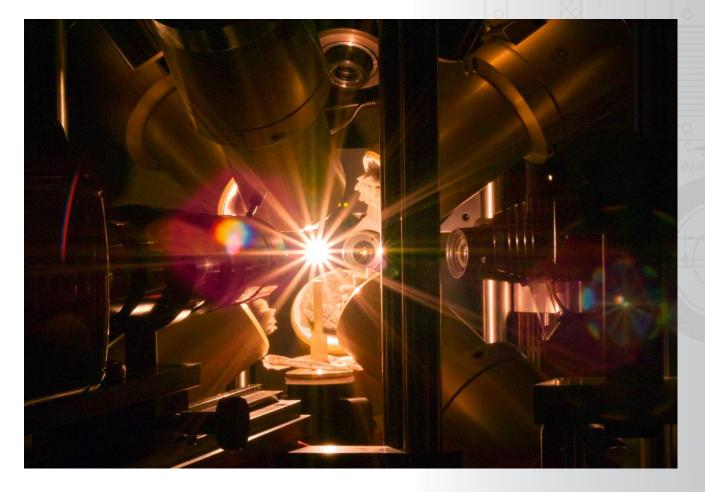
Product Description

Aero-Acoustic Levitator

Model 4.1

For investigation and processing of solids and liquids at very high temperatures, >3000°C.





PHYSICAL PROPERTY MEASUREMENTS, INC. 825 CHICAGO AVENUE, SUITE E EVANSTON, ILLINDIS USA 60202 TELEPHONE: 847 864 8509 FAX: 847 864 9114 EMAIL: PNORDINE@PPMEASUREMENTS.COM WWW.PPMEASUREMENTS.COM



Aero-Acoustic Levitator - Background and Applications

Liquids at very high temperatures occur in critical environments: aluminum fueled rocket exhaust, nuclear reactor accidents, volcanic eruptions, and in basic scientific investigations into the properties of materials. Temperatures in excess of 3000° Celsius can be of interest where no suitable containers are available. In fact, the discovery of inert containers for work at even lower temperatures is often the principal and most difficult problem to solve in experimental high temperature science. The Aero-Acoustic Levitator^{1,2} (AAL) provides containerless conditions for high temperature research. It enables well-controlled, contaminationfree investigation of liquid and solid materials at extreme temperatures.

Containerless conditions achieved with the AAL allow study of deeplyundercooled melts³⁻⁹ at temperatures far below the melting point. Novel glasses¹⁰⁻¹³ can be formed from melts that would otherwise crystallize upon cooling. Phase transitions under extreme conditions that may otherwise be missed are found by direct visual observation¹⁴⁻¹⁷. Well-controlled investigations of oxidation/reduction reactions¹⁸⁻²⁰ and phase diagrams²⁰ are possible. There are further possibilities for novel advances, such as surface tension and viscosity measurements by drop oscillation experiments^{21,22}, liquidus and melting point measurements¹⁶ that would otherwise be influenced by contaminants, optical property and emissivity measurements on liquids^{20,23-28}, synthesis of ultra-pure²⁹ and potentially single crystalline materials, and calorimetric measurements of thermodynamic properties. Together, such investigations will advance scientific understanding of the liquid state of matter and gain a deeper understanding of material properties under technologically-important conditions.

In AAL, levitation is by an aerodynamic force of an upward flowing gas jet stabilized by acoustic forces subject to feedback control from an optical position-sensing system. In combination with laser beam heating, stable and well-controlled levitation of solid and molten materials is obtained at temperatures limited only by material volatility. Extensive applications to oxide materials have been made. The AAL can be equipped with an inert shield gas flow or installed in a glove box for application to air-sensitive materials..



Aero-Acoustic Levitator - Features and Specifications

Features of the basic system are given below. AAL systems are built to order following discussion of special needs for the applications of interest.

- Laser beam heating and melting of levitated samples with fast optical pyrometry for temperature measurements.
- Operation with any involatile solid or liquid material sample, typically 0.25 to 0.35 cm diameter, and density up to at least 12 g/cc.
- Gas jet levitation in a three-axis acoustic system operated at 22 kHz.
- Electrically-heated aerodynamic levitation nozzle for use with air, oxygen, inert- or active-process gases. The gas is heated to stabilize laminar flow.
- Position sensing and sample velocity feedback controls acoustic standing waves to enhance sample stability.
- Acoustic forces control shape, spin, and can induce resonant oscillation of liquid drops.
- Video imaging provides well-resolved viewing of the levitated material under extreme radiance conditions.
- A fast video camera records sample rotation, oscillation, shape, and crystallization events, at kHz rates.
- The standard system has components integrated in a stand-alone frame. It can be configured for glove box operation.

Added features of the Model 4.1 AAL System

- Motor-operated axial positioning of three acoustic transducers. The phase difference of opposed transducers is kept at 180 to maintain coincident nodes from the direct and reflected outputs of the acoustic transducers.
- Increased temperature capability in the gas jet heater to obtain laminar jet flow at increased flow rates for operation with high density materials.
- Inert shield gas flow apparatus for work on air-sensitive materials.
- Motor-driven stinger for melting point measurements. For melting/liquidus studies by observing stinger-induced crystallization of liquids below, but not above the melting/liquidus temperature.
- Oscillating drop measurements for surface tension and viscosity measurements. Diode laser source, detector, and electronics, with data acquisition and operating software.



Instrument Dimensions

Levitator structure	Base	0.6 x 0.6 m (24″x 24″)
	Height	0.9 m (36″)
System structure	Base	1.4 x 1.6 m (55″ x 62″)
	Height	2.0 m (78″)
Total weight		500 kg (1100 lb)

Utility Requirements

Electrical (includes laser power)	
Cooling water for each of 2 lasers	
Gases for levitation up to	

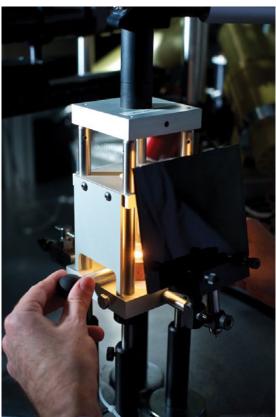
6 circuits, 240V, 30A 1000 liter/hour (4 gal/min) 10 liter/min (21 ft³/hour)

Dimensions and utility requirements are approximate. Other supply voltages and line frequencies are available.





Photograph of the Model 3.1 Aero-Acoustic Levitator system showing table-top levitator, CO_2 laser beam heating, rack-mounted electronics, and Vision Research fast camera.

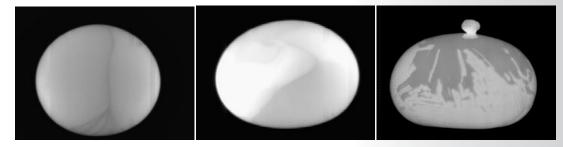




From the left:

Dennis Merkley (acoustics, project management), Paul Nordine (PPM President), Jeff Sickel (software) during AAL delivery in Germany³². Other team members not pictured here are James Rix (mechanical design) and John DeVos (electronics).

Laser Hearth melter³⁰ used for sample preparation



Photographs of levitated samplesLeft – liquid Al_2O_3 , Ta = 3200°C; Center - liquid HfO_2 , density \approx 9.6 g/cc Ta = 2910°C;Right – Solid Y_2O_3 phase transition, Ta = 2270°C.

Please contact PPM for discussion of your interest and needs. Additional information, including video of AAL experiments is at www.ppmeasurements.com



References to AAL and Non-Contact Experiments

- J.K.R. Weber, D.S. Hampton, D.R. Merkley, C.A. Rey, M.M. Zatarski and P.C. Nordine, "Aero-Acoustic Levitation - A method for containerless liquid phase processing at high temperatures," Rev. Sci. Instrum., 65, 456-465 (1994).
- J.K.R. Weber, J.J. Felten, B. Cho and P.C. Nordine, "Design and Performance of the Aero-Acoustic Levitator," J. Jpn. Soc. Microgravity Appl., 13, 27-35 (1996).
- J.K.R. Weber, C.D. Anderson, S. Krishnan and P.C. Nordine, "Solidification Behavior of Undercooled Liquid Aluminum Oxide," J. Am. Ceram. Soc., 78, 577-82 (1995).
- W.M. Kriven, M.H. Jilavi, D. Zhu, J.K.R. Weber, B. Cho, J.J. Felten and P.C. Nordine, "Synthesis and Microstructure of Mullite Fibers Grown from Deeply Undercooled Melts," Ceramic Microstructures '96, Eds. A.P. Tomsia and A. Glaesser, Ceramic Microstructure: Control at the Atomic Level, Plenum Press, NY, 1998, pp. 169-176.
- K. Nagashio, Y. Takamura and K. Kuribayashi, "Congruent Growth of NdBa₂Cu₃O₇₋₈ Superconducting Oxide from the Highly Undercooled Melt by Containerless Processing," Proc. PRICM3, Eds. M.A. Imam, R. DeNale, S. Hanada, Z. Zhong and D.N. Lee, 565-570 (1998).
- 6. K. Nagashio, Y. Takamura and K. Kuribayashi, "Coupled Growth in the Peritectic Nd-Ba-Cu-O System from Highly Undercooled Melt," Scripta Mater., 41, 1161-67 (1999).
- K. Nagashio, Y. Takamura, K. Kuribayashi and Y. Shiohara, "Microstructural Control of NdBa₂Cu₃O_{7.5} Superconducting Oxide from Highly Undercooled Melt by Containerless Processing," J. Cryst. Growth, 200, 118-25 (1999).
- K. Nagashio, K. Kuribayashi and Y. Takamura, "Phase Selection of Peritectic Phase in Undercooled Nd-based Superconducting Oxides," Acta Mater., 48, 3049-57 (2000).
- 9. K. Nagashio and K. Kuribayashi, "Rapid Solidifcation of Y₃Al₅O₁₂ Garnet from Hypercooled Melt," Acta Mater., 49, 1947-55 (2001).
- J.K.R. Weber, J.J. Felten, B. Cho, and P.C. Nordine, "Glass Fibers of Pure and Erbium- or Neodymium-doped Yttria-Alumina Compositions," Nature 393, 769-71 (1998).
- 11. I-Ching Lin, A. Navrotsky, J.K.R. Weber, and P.C. Nordine, "Thermodynamics of glass formation and metastable solidification of molten Y₃Al₅O₁₂," J. Non-Cryst. Solids, 243, 273-276 (1999).
- J.K.R. Weber, J.G. Abadie, A.D. Hixson, P.C. Nordine, and G.A. Jerman, "Glass Formation and Polyamorphism in Rare Earth Oxide-Alumina Compositions," J. Am. Ceram. Soc. 83, 1868-72 (2000).
- K. Nagashio, W.H. Hofmeister, D.E. Gustafson, A. Altgilbers, R.J. Bayuzick and K. Kuribayashi, "Formation of NdBa₂Cu₃O_{7-δ} Amorphous Phase by Combining Aero-Acoustic Levitation and Splat Quenching," J. Mater. Res., 16, 138-45 (2001).
- K. Nagashio, Y. Takamura and K. Kuribauashi, "Containerless Solidification of Peritectic and Eutectic Ceramics using Aero-Acoustic Levitator," Mater. Sci. Forum, 329/330, 173-78 (2000).
- 15. K. Nagashio, K. Kuribayashi and Y. Takamura, "Direct Crystallization of Y₃Fe₅O₁₂ Garnet by Containerless Solidification Processing," Metall. Trans.,42, 233-37 (2001).
- C. D. Anderson, W. H. Hofmeister, and R. J. Bayuzick, "Liquidus Temperatures in the Ti-Al System", Metall. Trans. 24A, 61-66 (1993).
- 17. C. D. Anderson, W. H. Hofmeister, and R. J. Bayuzick, "Solidification Kinetics and Metastable Phase Formation in Binary Ti-Al", Metall. Trans. 23A, 2699-2714 (1992).
- J.K.R. Weber, P.C. Nordine, K.C. Goretta, and R.B. Poeppel, "Effects of oxygen pressure on the structure of Y-Ba-Cu-O Materials formed by Containlerless Melting and Solidification," J. Mater. Res., 9, 1657-60 (1994).

- 19. R.F. Cooper, J.B. Fanselow, J.K.R. Weber, D.R. Merkley and D.B. Poker, "Dynamics of Oxidation of a Fe2+-bearing Aluminosilicate (Basaltic) Melt," Science, 274, 1173-76 (1996).
- 20. R.I. Sheldon, G.H. Rinehart, S. Krishnan and P.C. Nordine, "The Optical Properties of Liquid Cerium at 632.8 nm," Mater. Sci. Eng. B79, 113-122 (2001).
- J.W.S. Rayleigh, "On the Capillary Phenomena of Jets", Proceedings of the Royal Society of London, 29, 71-79 (1879).
- 22. H. Lamb, "On the Oscillations of a Viscous Liquid Globe", Proceedings of the London Math. Society, 13, 51-66 (1881).
- 23. S. Krishnan, C. D. Anderson, J. K. R. Weber, P. C. Nordine, W. H. Hofmeister, and R. J. Bayuzick, "Optical Properties and Spectral Emissivities at 632.8 nm in the Titanium-Aluminum System," Metall. Trans. 24A, 67-72 (1993).
- 24. Krishnan, S., J. K. R. Weber, R. A. Schiffman, P. C. Nordine, and R. A. Reed, "Refractive Index of Liquid Aluminum Oxide at 0.6328 µm," J. Am. Ceram. Soc. 74, 881 (1991).
- 25. J.K.R. Weber, S. Krishnan, C.D. Anderson and P.C. Nordine, "Spectral Absorption Coefficient of Liquid Aluminum Oxide from 0.385-0.780 μm," J. Am. Ceram. Soc., 78, 583-87 (1995).
- J.K.R. Weber, S. Krishnan and P.C. Nordine, "Effects of Melt Chemistry on the Spectral Absorption Coefficient of Liquid Aluminum Oxide," J. Am. Ceram. Soc., 78, 3067-3071 (1995).
- 27. Krishnan, S., J. K. R. Weber, C. D. Anderson, P. C. Nordine, and R. I. Sheldon, "Spectral Emissivity and Optical Properties at $\lambda = 632.8$ nm for Liquid Uranium and Zirconium at High Temperatures," J. Nucl. Mater. 203, 112-121 (1993).
- R.I. Sheldon, G.H. Rinehart, J.C. Lashley, C.E. Van Pelt, P.C. Nordine, S. Krishnan, J.K.R. Weber, "The optical properties of liquid plutonium at 632.8 nm", J. Nucl. Mater. 312, 207 211 (2003).
- 29. A.B. Biswas, J.K.R. Weber and P.C. Nordine, "Cr³⁺ Fluorescence in Containerless Melt-purified Aluminum Oxide" J. Mater. Res., 10, 1823-27 (1995).
- Weber, J.K.R., J.J. Felten and P.C. Nordine, "Laser hearth melt processing of ceramic materials," Rev. Sci. Instrum. 67, 522-524 (1996).
- 31. P.C. Nordine, J.K.R. Weber and J.G. Abadie, "Properties of high-temperature melts using levitation," Pure Appl. Chem., 72, 2127-36 (2000).
- 32. R. Telle, A. Kaiser, and P.C. Nordine, "Characterization of Non-Metallic Melts By Aero Acoustic Levitation", Proc. Intl. Tech. Conf. Refractories (2011).

